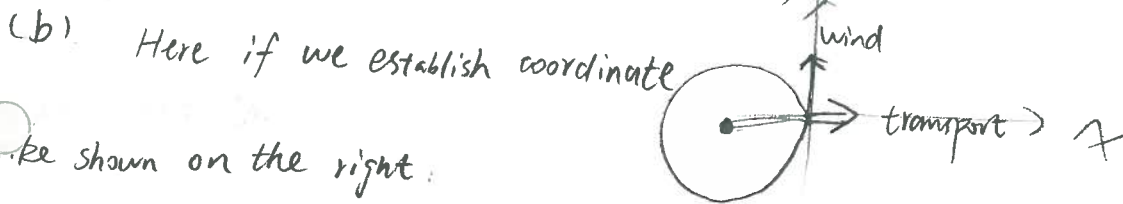
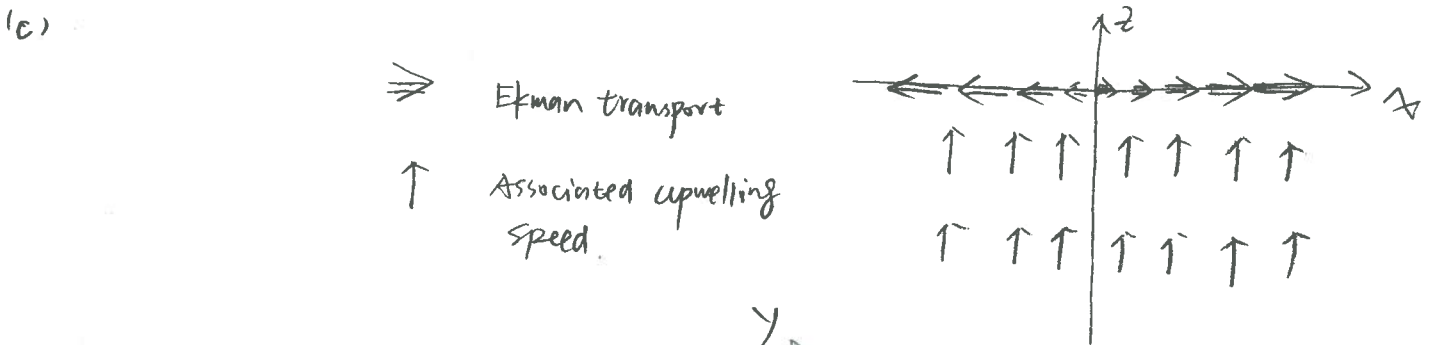
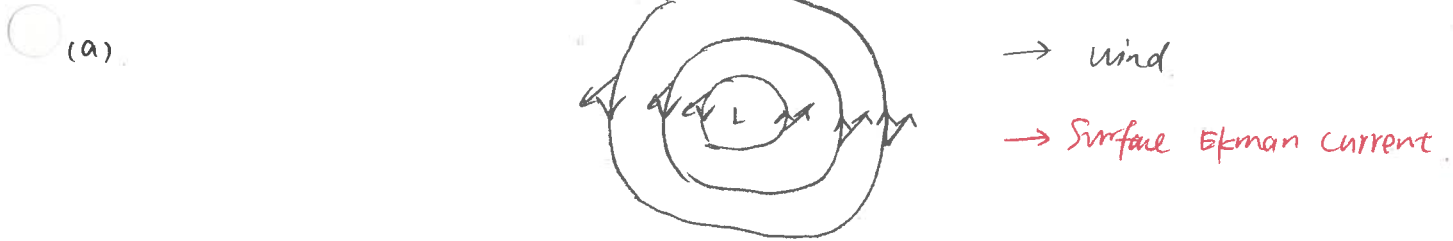


Answers for Revision questions of Nov. 22nd & Nov 29th. (By Peter Zhang)



then: $T_x = \frac{1}{\rho f} T_y = \frac{1}{\rho f} (\rho \alpha \nu \cdot C_d \cdot U^2) = \frac{1}{10^3 \cdot 10^{-4}} \cdot (1 \cdot 10^{-3} \cdot 50^2) = 25 \text{ m}^2/\text{s}$

And the total transport along the whole circle would be:

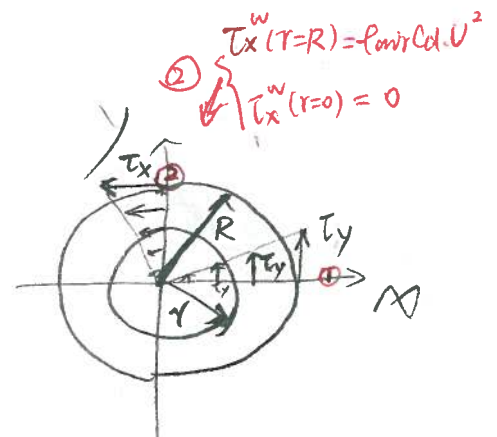
$T_x \cdot d = T_x \cdot 2\pi R = 25 \times 2 \times 3.14 \times 70 \times 10^3 = 4.71 \times 10^6 \text{ m}^3/\text{s}$

↑
circumference of this circle

(d) Since the surface shear stress varies linearly,

and $T_y^w(r=R) = \rho \alpha \nu \cdot C_d \cdot U^2 \leftarrow U=50 \text{ m/s}$, outer edge

① $T_y^w(r=0) = 0 \leftarrow$ No wind speed.



From the equation: $w_e(z=-D_E) = \frac{1}{\rho f} \left(\frac{\partial T_y^w}{\partial x} - \frac{\partial T_x^w}{\partial y} \right) = \frac{1}{\rho f} \cdot \left[\frac{\rho \alpha \nu \cdot C_d \cdot U^2}{R} - \frac{(-\rho \alpha \nu \cdot C_d \cdot U^2)}{R} \right]$

$$= \frac{1}{\rho f} \cdot \frac{2 \rho \omega r \cdot C_d \cdot V^2}{R} = \frac{1}{10^3 \cdot 10^{-4}} \cdot \frac{2 \times 1 \times 10^{-3} \times (50)^2}{30 \text{ km}} = 1.67 \times 10^{-3} \text{ m/s.}$$

$$= 144 \text{ m/day.}$$

2) From the conservation of potential

vorticity:

$$\frac{d}{dt}(P.V) = \frac{d}{dt} \left(\frac{s+f}{H} \right) = 0.$$

From the formula: $\left(\frac{b}{a}\right)' = \frac{b'a - a'b}{a^2}$

$$\Rightarrow \frac{\frac{d(s+f)}{dt} \cdot H - \frac{dH}{dt} \cdot (s+f)}{H^2} = 0.$$

$$\Rightarrow \boxed{\frac{dH}{dt}} = \frac{H}{s+f} \cdot \frac{d(s+f)}{dt}$$

$-w_e(\text{bottom})$

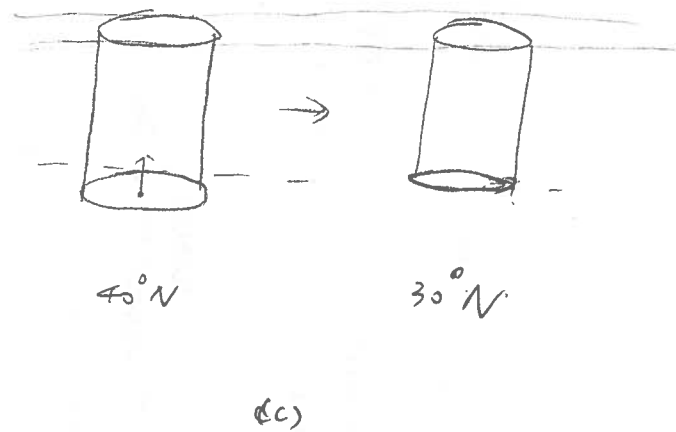
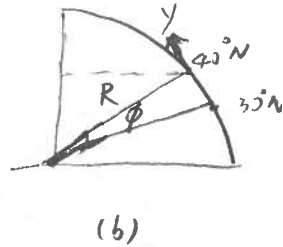
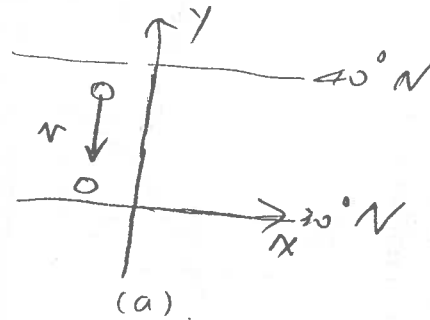
$$\Rightarrow w_e(\text{bottom}) = \frac{-H}{s+f} \cdot \left(\frac{ds}{dt} + \frac{df}{dt} \right) = - \frac{H}{s+f} \cdot \frac{df}{dt}$$

Also, $f = 2\Omega \sin\phi \Rightarrow \frac{df}{dt} = 2\Omega \cdot \cos\phi \cdot \frac{d\phi}{dt} = 2\Omega \cos\phi \cdot \frac{d\psi}{dt} \cdot \frac{1}{R} = \frac{2\Omega \cos\phi}{R} \cdot \psi$

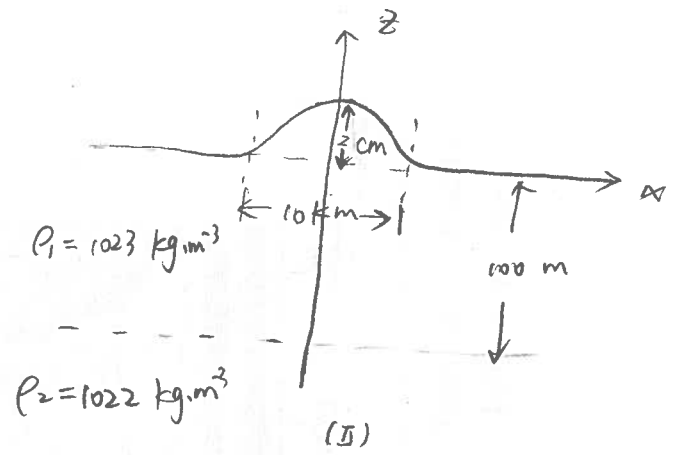
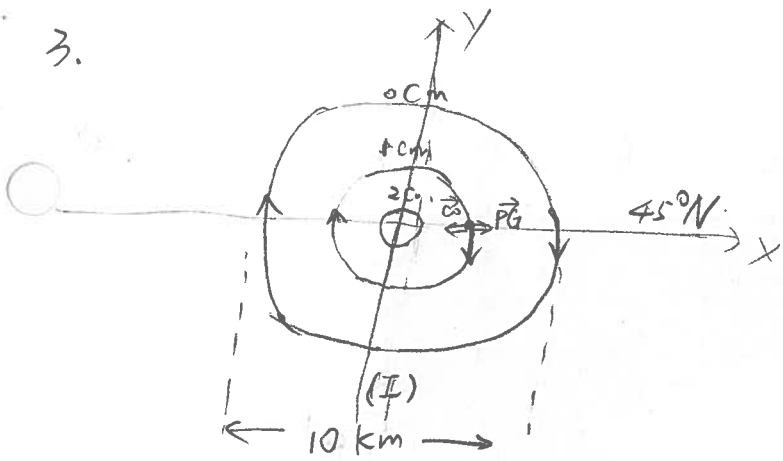
$$\Rightarrow w_e(\text{bottom}) = - \frac{H}{s+f} \cdot \frac{2\Omega \cos\phi}{R} \cdot \psi$$

Here in this case: $s = -0.1 f$; $H = 1000 \text{ m}$; $\Omega = 7.29 \times 10^{-5} \text{ rad/s}$; $\psi = -0.5 \text{ m/s}$
 $\phi = 35^\circ \text{ N}$ $R = 6370 \text{ km}$

$$\Rightarrow w_e(\text{bottom}) = - \frac{H}{0.9 \sin\phi} \cdot \frac{\cos\phi}{R} \cdot \psi = +1.25 \times 10^{-4} \text{ m/s} \quad \text{rise upward.}$$



3.

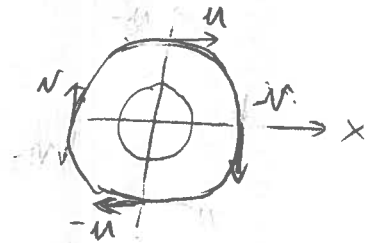


(a). Shown in figure (I)

$$fv = \frac{1}{\rho} \frac{\partial p}{\partial x} \Rightarrow v = \frac{1}{\rho f} \frac{\partial p}{\partial x} = \frac{g}{f} \cdot \frac{\partial \eta}{\partial x} = \frac{10}{10^4} \cdot \frac{0 - 2 \text{ cm}}{5 \text{ km}} = -4 \times 10^{-3} \text{ (m/s)}$$

(b). Relative vorticity $S = \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$

$$= \frac{-2v}{2R} - \frac{2u}{2R}$$



Also, $|u| = |v|$

$$\Rightarrow S = -\frac{2u}{R} = -\frac{2 \times 4 \times 10^{-3}}{5 \text{ km}} = -1.6 \times 10^{-6} \text{ (1/s)}$$

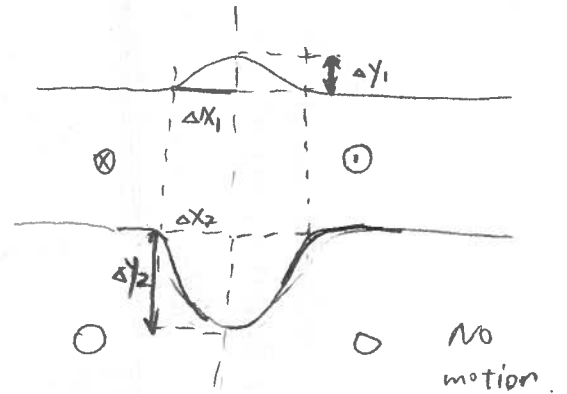
(c). Using Margule's equation:

$$v_2 = -v_1 \cdot \left(\frac{\rho_1}{\rho_2 - \rho_1} \right)$$

$$\Rightarrow \frac{\Delta y_2}{\Delta x_2} = -\frac{\Delta y_1}{\Delta x_1} \cdot \frac{1022 \text{ kg/m}^3}{(1023 - 1022) \text{ kg/m}^3}$$

$$\Rightarrow \Delta y_2 = -\frac{\Delta x_2}{\Delta x_1} \cdot \Delta y_1 \cdot 1022$$

$$\text{Also, } \Delta x_1 = \Delta x_2 \Rightarrow \Delta y_2 = -1022 \Delta y_1 = -1022 \times 2 \text{ cm} = -2044 \text{ cm} = -20.44 \text{ m.}$$



(d) If $45^\circ N \rightarrow 30^\circ N$

$f \downarrow$

$\frac{d}{dt} \left(\frac{S+f}{H} \right) = 0 \Rightarrow$ Either $S \uparrow$, if H constant.

Or $H \downarrow$, if S constant.

4) (a) $\beta M_y = \frac{\partial \tau_y^w}{\partial x} - \frac{\partial \tau_x^w}{\partial y} = \text{Curl}(\vec{\tau}^w)$

$\Rightarrow M_y = \frac{1}{\beta} \left(\frac{\partial \tau_x^w}{\partial y} \right) = \frac{1}{\beta} \cdot \left[+ 0.2 \cdot \frac{\pi}{L_y} \sin\left(\frac{\pi \cdot y}{L_y}\right) \right] = \frac{0.2 \cdot \pi}{\beta \cdot L_y} \sin\left(\frac{\pi}{L_y} \cdot y\right)$

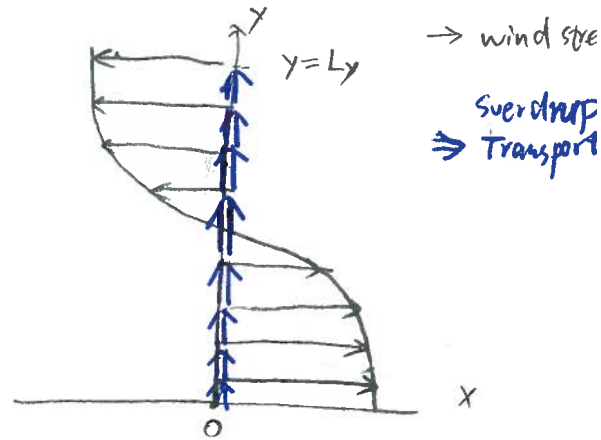
Also, $M_y = \rho_0 \cdot \int_H^0 \bar{v} dz = \rho_0 \cdot \bar{v} \cdot H$

↑
Assume the vertically averaged velocity \bar{v} .

$\Rightarrow \bar{v} = \frac{M_y}{\rho_0 H} = \frac{0.2 \pi}{\rho_0 H \cdot \beta \cdot L_y} \cdot \sin\left(\frac{\pi}{L_y} \cdot y\right)$

when y varies from $y=0$ to $y=L_y$.

\bar{v} is positive all the time.



(b) Ignoring friction, we would have.

$\beta M_y = \text{Curl}(\vec{\tau}^w)$

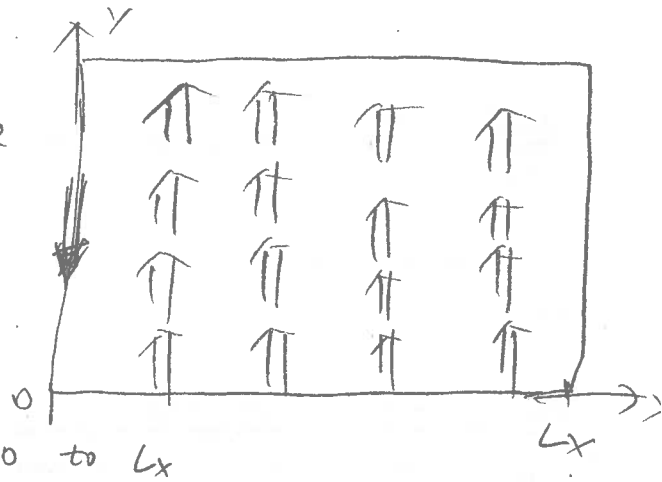
Also, $\Delta Q = \Delta \left[\frac{S+f}{H} \right] = \frac{\Delta S}{H} \propto \Delta \text{Curl}(\vec{\tau}^w)$

$\Rightarrow \Delta(\beta M_y) = \Delta(\text{Curl}(\vec{\tau}^w)) \propto \frac{\Delta S}{H}$

$\Rightarrow \Delta \bar{v} \propto \Delta S \propto \Delta Q$

(C) Suppose the return flow is along the western boundary (only assumption)

then the transport would be the integral of M_y ~~over~~ along the x direction from 0 to L_x



(conservation \Rightarrow All the flow toward north has to equal all the flow toward south)

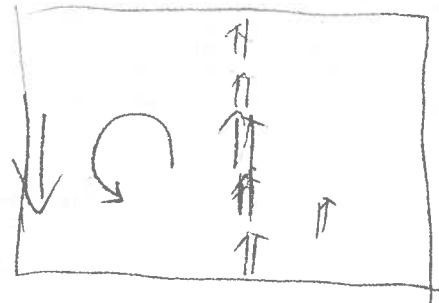
$$\Rightarrow M_{total(y)} = \int_0^{L_x} M_y \cdot dx = \int_0^{L_x} \frac{1}{\beta} \cdot \text{curl}(\vec{v}^w) \cdot dx = \frac{L_x}{\beta} \cdot \text{curl}(\vec{v}^w)$$

$$= \frac{L_x}{\beta} \cdot \left(-\frac{\partial v^w}{\partial y}\right) = \frac{0.2 \pi \cdot L_x}{\beta L_y} \cdot \sin\left(\frac{\pi}{L_y} \cdot y\right)$$

(d) Western Boundary Wall.

why?

Balance of vorticity input to the whole system.



So friction \curvearrowright

\leftarrow sink of vorticity

could balance wind curl \curvearrowright

\leftarrow source of vorticity

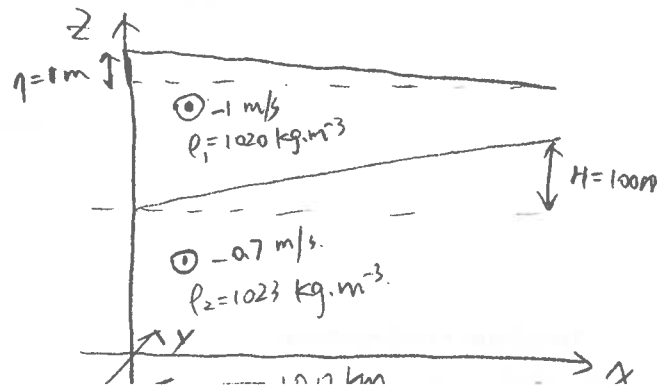
5) a) Establish one coordinate like shown on right:

For surface geostrophic current:

$$f v_1 = \frac{1}{\rho_1} \frac{\partial p}{\partial x} \Rightarrow v = \frac{g}{f} \frac{\partial \eta}{\partial x} = \frac{10}{10^{-4}} \cdot \frac{-8 \text{ m}}{100 \text{ km}} = -1 \text{ (m/s)}$$

For lower layer geostrophic current:

$$f v_2 = \frac{1}{\rho_2} \frac{\partial p}{\partial x} \Rightarrow \rho_2 f v_2 = \frac{\partial p_1}{\partial x} + \frac{\rho_2 \rho_1}{\rho_1} g \frac{\partial z}{\partial x} = \rho_1 g v_1 + \rho_2 g v_2$$

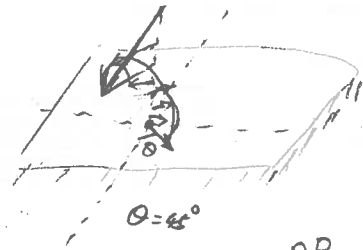


$$\Rightarrow v_z = \frac{\rho_1 g z_1 + \Delta \rho g z_2}{\rho_2 f} = \frac{1020 \times 10 \times \left(-\frac{1 \text{ m}}{100 \text{ km}}\right) + 3 \cdot 10 \cdot \frac{100 \text{ m}}{100 \text{ km}}}{1023 \cdot 10^{-4}}$$

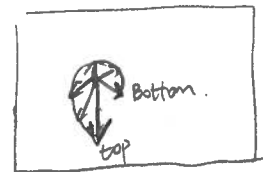
$$= -0.7 \text{ m/s.}$$

(b) Bottom Ekman Layer.

Shown on the right.



OR.



(c) If the pressure gradient is exactly canceled in the

lower layer, which means no motion in lower layer, then:

From Monge's equation:

$$\hat{v}_z = -\hat{v}_1 \cdot \left(\frac{\rho_1}{\rho_2 - \rho_1} \right) = -\frac{1}{100 \text{ km}} \cdot \frac{1020}{3} = \frac{340 \text{ m}}{100 \text{ km}}$$

$$\Rightarrow H_1 = \hat{v}_z \cdot \Delta X = \frac{340 \text{ m}}{100 \text{ km}} \times 100 \text{ km} = 340 \text{ m.}$$

d) There would be no flow in the lower layer, so the bottom

Ekman layer would not exist. (or the flow is zero)

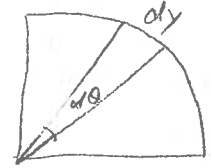
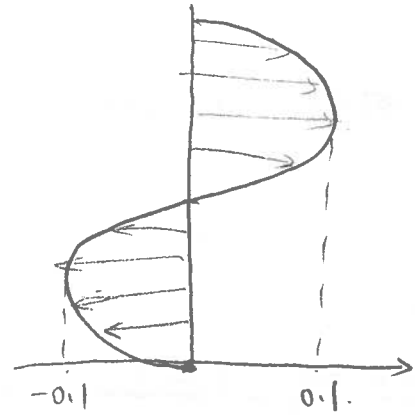
6). $T_x = 0.1 \cdot \sin(\text{latitude}/10)$

a). From: $W_e(z=-D_E) = \frac{1}{\rho f} \left(\frac{\partial T_y^w}{\partial x} - \frac{\partial T_x^w}{\partial y} \right)$

$$= \frac{1}{\rho f} \cdot \left(-\frac{\partial T_x}{\partial y} \right)$$

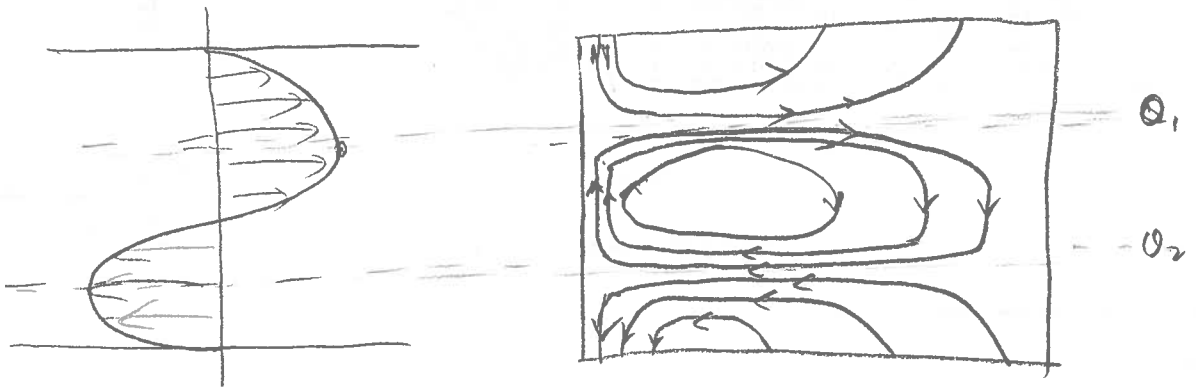
$$= \frac{1}{\rho f} \cdot \left[-\frac{0.1}{10} \cdot \cos(\text{latitude}/10) \cdot \frac{d(\text{latitude})}{dy} \right] \rightarrow \frac{1}{R}$$

$$= -\frac{10^{-2}}{\rho R f} \cos(\text{latitude}/10)$$



$$\frac{dy}{d\theta} = \frac{dx}{d(\text{latitude})} = R$$

b).



$$\theta_1 = \frac{3}{2}\pi \cdot 10 = 15\pi \approx 47.1^\circ$$

$$\theta_2 = \frac{\pi}{2} \cdot 10 = 5\pi \approx 15.7^\circ$$

c). $\beta M_y = \text{curl}(\vec{T}^w) \Rightarrow M_y = \frac{1}{\beta} \text{Curl} \vec{T}^w = -\frac{1}{\beta} \cdot \frac{\partial T_x^w}{\partial y} = -\frac{10^{-2}}{R} \cos(\text{latitude}/10)$

when $\text{Curl}(\vec{T}^w)$ is maximum $\Rightarrow M_y$ maximum.

when - - - is minimum $\Rightarrow M_y$ minimum.

Proportional